# Clean Final Draft IRM Report Appendices

# New York Control Area Installed Capacity Requirement



## For the Period May 2025 To April 2026



# November 25, 2024

New York State Reliability Council, LLC Installed Capacity Subcommittee

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# **Appendix A**

# **NYCA Installed Capacity Requirement Reliability Calculation Models and Assumptions**

**Description of the GE MARS Program: Load, Capacity, Transmission, Outside World Model, and Assumptions**

## <span id="page-7-0"></span>**A. Reliability Calculation Models and Assumptions – Appendix A**

The reliability calculation process for determining the New York Control Area (NYCA) Installed Reserve Margin (IRM) requirement utilizes a probabilistic approach. This technique calculates the probabilities of outages of generating units, in conjunction with load and transmission models, to determine the number of days per year of expected capacity shortages. The General Electric Multi-Area Reliability Simulation (GE-MARS) is the primary computer program used for this probabilistic analysis. The result of the calculation for "Loss of Load Expectation" (LOLE) provides a consistent measure of system reliability. The various models used in the NYCA IRM calculation process are depicted in Figure A.1 below.

Table A.1 lists the study parameters, the source for the study assumptions, and where the assumptions are described in Appendix A. Finally, section A.3 compares the assumptions used in the 2024-2025 and 2025-2026 IRM reports.



## <span id="page-7-1"></span>**Figure A.1 NYCA ICAP Modeling**

## **Table A.1 Modeling Details**

<span id="page-8-0"></span>

<span id="page-8-1"></span><sup>&</sup>lt;sup>1</sup> 2024 Load and Capacity Data report ("2024 Gold Book"),

http://www.nyiso.com/public/markets\_operations/services/planning/documents/index.jsp

## <span id="page-9-0"></span>**A.1 GE-MARS**

As the primary probabilistic analysis tool used for establishing NYCA IRM requirements, the GE-MARS program includes a detailed load, generation, and transmission representation for 11 NYCA Zones, as well as the four external Control Areas (Outside World Areas) interconnected to the NYCA (see Section A.3 for a description of these Zones and Outside World Areas).

A sequential Monte Carlo simulation forms the basis for GE-MARS. The Monte Carlo method provides a fast, versatile, and easily expandable program that can be used to fully model many different types of generation, transmission, and demand-side options. GE-MARS calculates the standard reliability indices of daily and hourly LOLE (event-days/year and event-hours/year) and Loss of Energy Expectation (LOEE in MWh/year). The use of sequential Monte Carlo simulation allows for the calculation of time-correlated measures such as frequency (outages/year) and duration (hours/outage). The program also calculates the need for initiating Emergency Operating Procedures (EOPs), expressed in days/year (see Section A.3.5).

In addition to calculating the expected values for the reliability indices, GE-MARS also produces probability distributions that show the actual yearly variations in reliability that the NYCA could be expected to experience. In determining NYCA reliability, there are several types of randomly occurring events that must be taken into consideration. Among these are the forced outages of generating units and transmission capacity. Monte Carlo simulation models the effects of such random events. Deviations from the forecasted loads are captured using a load forecast uncertainty model.

Monte Carlo simulation approaches can be categorized as "non-sequential" and "sequential." A non-sequential simulation process does not move through time chronologically or sequentially, but rather considers each hour independent of every other hour. Because of this, non-sequential simulation cannot accurately model issues that involve time correlations, such as maintenance outages, and cannot be used to calculate time-related indices such as frequency and duration.

Sequential Monte Carlo simulation (used by GE-MARS) steps through the year chronologically, recognizing the status of equipment is not independent of its status in adjacent hours. Equipment forced outages are modeled by taking the equipment out of service for contiguous hours, with the length of the outage period being determined from the equipment's mean time to repair. Sequential simulation can model issues of concern that involve time correlations and can be used to calculate indices such as frequency and duration. It also models transfer limitations between individual areas.

Because the GE-MARS program is based on a sequential Monte Carlo simulation, it uses state transition rates, rather than state probabilities, to describe the random forced outages of the thermal units. State probabilities give the probability of a unit being in a given capacity state at any particular time and can be used if one assumes that the unit's capacity state for a given hour is independent of its state at any other hour. Sequential Monte Carlo simulation recognizes the fact that a unit's capacity state in any given hour is dependent on a given state in previous hours and influences its state in future hours. It thus requires additional information that is contained in the transition rate data.

For each unit, a transition rate matrix is input that shows the transition rates to go from each capacity state to each other capacity state. The transition rate from state A to state B is defined as the number of transitions from A to B per unit of time in state A (Equation A.1).

#### **Equation A.1 Transition Rate Definition**

 $\textit{Transition}\ (\textit{A to B}) = % \begin{cases} f(x) & \text{if } x \leq x \leq 1, \\ 0 & \text{if } x \leq x \leq 2. \end{cases} \label{eq:transit}$ Number of Transitions from A to B Total Time in State A

<span id="page-10-0"></span>Table A.2 shows the calculation of the state transition rates from historic data for one year. The "Time-in-State Data" shows the amount of time that the unit spent in each of the available capacity states during the year; the unit was on planned outage for the remaining 760 hours of the year. The "Transition Data" shows the number of times that the unit transitioned from each state to each other state during the year. The "State Transition Rates" can be calculated from this data. For example, the transition rate from state 1 to state 2 equals the number of transitions from 1 to 2 divided by the total time spent in state 1 (Equation A.2).

#### <span id="page-10-1"></span>**Equation A.2 Transition Rate Calculation Example**

 $\textit{Transition} \ (1 \ to \ 2) =$ (10 Transitions)  $\frac{5,000 \text{ Hours}}{5,000 \text{ Hours}}$  = 0.0002

<span id="page-11-0"></span>

## **Table A.2 State Transition Rate Example**

From the state transition rates for a unit, the program calculates the two important quantities that are needed to model the random forced outages on the unit: the average time that the unit resides in each capacity state, and the probability of the unit transitioning from each state to each other state.

Whenever a unit changes capacity states, two random numbers are generated. The first is used to calculate the amount of time that the unit will spend in the current state; it is assumed that the time in a state is exponentially distributed, with a mean as computed from the transition rates. This time in state is added to the current simulation time to calculate when the next random state change will occur. The second random number is combined with the state transition probabilities to determine the state to which the unit will transition when it leaves its current state. The program thus knows for every unit on the system, its current state, when it will be leaving that state, and the state to which it will go next.

Each time a unit changes state, because of random state changes, the beginning or ending of planned outages, or mid-year installations or retirements, the total capacity available in the unit's area is updated to reflect the change in the unit's available capacity. This total capacity is then used in computing the area margins each hour.

## **A.1.1 Error Analysis**

An important issue in using Monte Carlo simulation programs such as GE-MARS is the number of years of artificial history (or replications) that must be created to achieve an acceptable level of statistical convergence in the expected value of the reliability index of interest. The degree of statistical convergence is measured by the standard deviation of the estimate of the reliability index that is calculated from the simulation data.

The standard deviation has the same physical units (*e.g.,* days/year) as the index being estimated, and thus its magnitude is a function of the type of index being estimated. Because the standard deviation can assume a wide range of values, the degree of convergence is often measured by the standard error, which is the standard deviation of the estimated mean expressed as a per unit of the mean.

Convergence can also be expressed in terms of a confidence interval that defines the range in which you can state, with a given level of confidence that the actual value falls within the interval. For example, a range centered on the mean of two standard deviations in each direction (plus and minus) defines a confidence interval of 95%.

For this analysis, the Base Case required 1,050 replicationsto converge to a standard error of 0.05 and required 4,236 replications to converge to a standard error of 0.025. For our cases, the model was run to 4,250 replications at which point the daily LOLE of 0.100 Event-Days/year for NYCA was met with a standard error less than 0.025. The confidence interval at this point ranges from 24.3% to 24.7%. An IRM of 24.4% is in full compliance with the NYSRC Resource Adequacy rules and criteria (see Base Case Study Results section).

#### **A.1.2 Conduct of the GE-MARS analysis**

The study was performed using Version 4.14.2179 of the GE-MARS software program. This version has been benchmark tested by the NYISO.

The current base case is the culmination of the individual changes made to last year's base case. Each change, however, is evaluated individually against last year's base case. The LOLE results of each of these pre-base case simulations are reviewed to confirm that the reliability impact of the change is reasonable and explainable.

General Electric was asked to review the input data for errors. They have developed a program called "Data Scrub" which processes the input files and flags data that appears to be out of the ordinary. For example, it can identify a unit with a forced outage rate significantly higher than all the others in that size and type category. If something is found, the NYISO reviews the data and either confirms that it is correct as is or institutes a correction. The results of this data scrub are shown in Section A.4.

The top three summer peak loads of all Areas external to NYCA are aligned to be on the same days as that of NYCA, even though they may have historically occurred at different times. This is a conservative approach, using the assumption that peak conditions could be the result of a widespread heat wave. This would result in reducing the amount of assistance that NYCA could receive from the external Areas.

## <span id="page-13-0"></span>**A.2 Methodology**

The 2025-2026 IRM study continues to use the Unified Methodology that simultaneously provides a basis for the NYCA installed reserve requirements and the preliminary locational installed capacity requirements (referred to as related Minimum Locational Capacity Requirements or "MLCRs"). The IRM/MLCR characteristic consists of a curve function, "a knee of the curve" and straight-line segments at the asymptotes. The curve function is represented by a quadratic (second order) curve which is the basis for the Tan 45 inflection point calculation. Inclusion of IRM/MLCR point pairs remote to the "knee of the curve" may impact the calculation of the quadratic curve function used for the Tan 45 calculation.

The procedure for determining the best fit curve function used for the calculation of the Tan 45 inflection point to define the base case requirement is based on the following methodology:

- 1) Start with all points on IRM/MLCR characteristic.
- 2) Develop regression curve equations for all different point to point segments consisting of at least four consecutive points.
- 3) Rank all the regression curve equations based on the following:
	- Sort regression equations with highest R2.
	- Remove any equations which show a negative coefficient in the first term. This is the constant labeled 'a' in the quadratic equation:  $ax^2 + bx + c$
	- Ensure the calculated IRM is within the selected point pair range (*e.g.*, if the curve fit was developed between 14% and 18% and the calculated IRM is 13.9%, the calculation is invalid).
	- In addition, there must be at least one statewide reserve margin point to the left and right of the calculated Tan 45 point.
	- Determine that the calculated IRM and corresponding MLCR do not violate the 0.1 Event-Days/year LOLE criteria.
	- Check results to determine that they are consistent with visual inspection methodology used in past years' studies.

This approach identifies the quadratic curve functions with highest  $R^2$  correlations as the

basis for the Tan 45 calculation. The final IRM is obtained by averaging the Tan 45 IRM points of the New York City and Long Island curves. The Tan 45 points are determined by solving for the first derivatives of each of the "best fit" quadratic functions as a slope of -1. Lastly, the resulting MLCR values are identified.

## <span id="page-14-0"></span>**A.3 Base Case Modeling Assumptions**

## **A.3.1 Load Model**

<span id="page-14-1"></span>

#### **Table A.3 Load Model**

## **A.3.2 Peak Load Forecast Methodology**

The procedure for preparing the IRM forecast is very similar to that described in the NYISO Load Forecasting Manual for the ICAP forecast. The NYISO and Transmission Owners developed regression models to evaluate the relationship between regional weather and Transmission District summer weekday peak loads, using data from the summer of 2024 and other recent summers as needed. The resulting estimates of weather response (*i.e.*, the MW increase in load per degree of increase in the weather variable) by Transmission District were used to develop 2024 Transmission District weather adjustments, which normalize the peaks to typical summer peak weather conditions. For purposes of the IRM and ICAP forecasts, the NYISO evaluates the system peak load that occurs during nonholiday weekdays in July and August. In 2024, the system peak load during this period was on July 8<sup>th</sup>, Hour Beginning 17. The system peak load of 28,895.0 MW is shown by Transmission District in Table A.4 (col. 2). The total MW adjustment (col. 3), including the weather adjustment, and estimated demand response and municipal self-generation impacts were added to the system peak, producing the 2024 weather normalized peak load of 31,327.0 MW (col. 4). Load and weather data from other summer 2024 high load days were considered in the determination of final 2024 Transmission District weather adjustments for the 2025-2026 IRM forecast.

Several Transmission Owners developed updated estimates of the Regional Load Growth Factor (RLGF) for their territories, while others did not. The RLGF represents the ratio of forecasted 2025 summer peak load to the 2024 weather normalized peak, based on the anticipated load growth or decline in the territory (excluding large load projects). Summer peak load growth rates from the 2024 Gold Book forecast and other NYISO analyses were used to determine RLGFs for those Transmission Owners that did not provide updates. The final RLGFs (col. 6) were reviewed by the NYISO and discussed with the Transmission Owners as needed. The 2025 forecast before adjustments (col. 7) is the product of the 2024 weather normalized peaks excluding large loads and the RLGFs. Summer 2025 large load projections are added in column 8. The resulting sum (col. 9) represents the 2025 IRM coincident peak forecast of 31,479.1 MW before Behind-the-Meter Net Generation (BTM:NG) adjustments. This forecast is a 0.5% decrease relative to the 2025 forecast from the 2024 Gold Book. For purposes of modeling in the IRM study, the forecast of BTM:NG resource load is added in column 10, producing a total forecast of 31,649.7 MW inclusive of BTM:NG load (col. 11).

The Locality forecasts are reported in the second table below. These forecasts are the product of the weather normalized coincident peak load in the Locality, the noncoincident to coincident peak (NCP to CP) ratio in the Locality, and the RLGF(s) of the Transmission District(s) in the Locality, plus any applicable large load growth in the Locality. The Locality NCP to CP ratios were calculated using the historical 15-year ratio (excluding outlier years). The Locality forecasts of 11,043.9 MW (Zone J), 5,092.1 MW (Zone K), and 15,205.1 MW (G-J Locality), inclusive of BTM:NG loads, are shown in column 11.

The third table below shows the 2024 non-coincident peak load forecast by Zone. Zonal coincident peak forecasts were generally derived using sub-zonal load shares (Transmission District to Zone), based upon peak and near-peak load hours from recent summers. Zonal non-coincident peak forecasts were calculated by multiplying the

coincident peak forecast by the Zonal NCP to CP ratios. The Zonal forecasts shown below include the projected impacts of BTM:NG and large load projects.

The peak load forecasts, along with the regression models, weather adjustments, RLGFs, zonal load shares, and NCP to CP ratios used to derive them were discussed and approved by the NYISO Load Forecasting Task Force (LFTF) and the NYSRC Installed Capacity Subcommittee (ICS). The LFTF recommended the Final 2025 Peak Load Forecast presented below to the NYSRC. The ICS approved the Final 2025 Peak Load Forecast for use in the 2025-2026 IRM study.

<span id="page-16-0"></span>![](_page_16_Picture_708.jpeg)

#### **Table A.4 2025 Final NYCA Peak Load Forecast – Coincident Peak**

#### **Table A.5 2025 Final NYCA Peak Load Forecast – Locality Peaks**

<span id="page-16-1"></span>![](_page_16_Picture_709.jpeg)

<span id="page-16-2"></span>**Table A.6 2025 Final NYCA Peak Load Forecast – Zonal Peaks**

![](_page_17_Picture_179.jpeg)

### **Zonal Load Forecast Uncertainty**

The load forecast uncertainty (LFU) models were not updated in 2024, and the LFU multipliers used in the 2024-2025 IRM study are retained in the 2025-2026 IRM study. Each year, the NYISO and the applicable Transmission Owners review load and weather data from the most recent summer and winter to determine whether updated LFU models are needed. Seasonal peak temperatures were below normal in summer 2023, and well below normal in winter 2023-2024. Since peak temperatures were below normal in these two seasons, there was no additional information to benefit the fit of load to the extreme upper-bin weather conditions impactful to resource adequacy modeling, and the LFU models were not updated.

The current LFU models were developed during the spring of 2023. The NYISO and pertinent Transmission Owners developed updated load-weather regression models inclusive of summer 2022 data. As with recent IRM studies, the equal-area approach was used to determine the reference temperatures of each of the seven LFU bins, which reflect the assumed normal distribution of the weather variable. This was done by setting the Z-value equal to the location of the midpoint of the area of each bin.

## *Review of Load-Weather Relationship*

Regression models were developed for all LFU modeling regions (Zones A-E, Zones F&G, Zones H&I, Zone J, and Zone K) to establish the recent load-weather relationship. The NYISO developed models for the Zones A-E and Zones F&G regions. Models for the Zones H&I and Zone J areas were developed in conjunction with Con Edison. The Zone K model was developed by LIPA and reviewed by the NYISO. The NYISO developed a system-level winter LFU model reflecting the load-weather relationship observed during the 2022- 2023 winter. All model results were presented to and reviewed by the NYISO Load Forecasting Task Force (LFTF) and NYSRC Installed Capacity Subcommittee (ICS). The ICS approved the 2023 LFU model results for use in the 2024-2025 IRM study. Due to the considerations noted above, primarily the mild peak weather during the recent summer and winter seasons, the resulting LFU multipliers are retained for the 2025-2026 IRM study.

The NYISO regional summer models established the load-weather relationship through polynomial regressions (generally 3<sup>rd</sup> order, or cubic). Pooled models using 2019, 2021, and 2022 summer data were developed. Multiple model structure combinations were

investigated for each region. The optimal pooled model was selected for each LFU area based on statistical model accuracy and the resulting weather sensitivity. The weather distribution used to define the LFU bin reference temperatures was calculated using 30 years of system peak-producing weather days. This distribution was applied to the loadweather relationship established by the selected regression models to calculate the LFU multipliers for each area. The LIPA Zone K splined linear model utilized data from the 2013 through 2022 summers.

The NYCA winter model utilized a  $2^{nd}$  order polynomial regression fit through winter 2018-2019, 2021-2022, & 2022-2023 load and weather data. The winter LFU model used the winter weather variable developed as part of the LFU Phase 3 analyses, based on temperature and wind speed.

The 2025-2026 IRM study LFU multipliers are presented in Table A.7. The rows list the seven bin levels and their probability of occurrence, along with the associated per-unit load multipliers by LFU area. These results are presented graphically in Figure A.2.

![](_page_18_Picture_62.jpeg)

#### <span id="page-18-0"></span>**Table A.7 2025-2026 IRM Study Summer and Winter Load Forecast Uncertainty Multipliers**

#### **Figure A.2** Sumer **LFU Distributions**

<span id="page-19-0"></span>![](_page_19_Figure_1.jpeg)

*Additional Discussion on the 2025-2026 LFU Models* 

The LFU models measure the load response to weather at high peak-producing temperatures and describe the variability in peak-day load caused by the uncertainty in peak-day weather. Other sources of uncertainty such as economic growth are not captured in LFU modeling. However, economic uncertainty is relatively small compared to temperature uncertainty one year ahead. As a result, the LFTF, the NYISO, and the ICS have agreed that it is sufficient to confine the LFU one year ahead to weather alone.

LFU multipliers are largely driven by the slope of load vs. temperature, or the weather response of load. If the weather response of load increases, the slope of load vs. temperature will increase, and the upper-bin LFU multipliers (Bins 1-3) will increase. Conversely, if the weather response of load decreases, upper-bin LFU multipliers will decrease.

The Con Edison and Orange & Rockland peak load forecasts are based on peak weather conditions with a 1-in-3 probability of occurrence (67th percentile). All other Transmission Owners design their forecasts at a 1-in-2 probability of occurrence (50th percentile). The resulting design conditions are 50th percentile for the Zones A-E and Zone K LFU areas, above 50<sup>th</sup> percentile for Zones F&G and Zones H&I, and 67<sup>th</sup> percentile for Zone J. The NYCA aggregate design condition reflected in the winter LFU multipliers is the 57<sup>th</sup> percentile.

### *LFU Bin Z-Values*

Beginning with the LFU models used in the 2022-2023 IRM study, LFU bin centers are based on Z-values which divide the area of each bin equally. In prior LFU modeling, bin centers were defined using the x-axis, equidistant from the upper and lower bounds of each bin based on the Z-value. The equal-area Z-values reflect an improved representation of the LFU multiplier's probability of occurrence. The comparison between equidistant and equal area based bin structure is shown in Figure A.3.

<span id="page-20-0"></span>![](_page_20_Figure_3.jpeg)

## **Figure A.3 Bin Centers (Equidistant v. Equal Area)**

## *Review of Historical Zonal Load Shapes for Load Bins*

Beginning with the 2014-2015 IRM study, multiple years of historical load shapes were assigned to the load forecast uncertainty bins. Three historical years were selected from those available, as discussed in the NYISO's 2013 report, 'Modeling Multiple Load Shapes in Resource Adequacy Studies'. The year 2007 was assigned to the lowest five bins (from

cumulative probability 0% to 93.32%). The year 2002 was assigned to the second highest bin, with a probability of 6.06%. The year 2006 was assigned to the highest bin (bin 1), with a probability of 0.62%.

Following the completion of the LFU Phase 2 analyses in 2022, the NYISO recommended and the ICS approved the use of the 2013, 2017, and 2018 load shapes beginning with the 2023-2024 IRM study.

A key finding of LFU Phase 2 was that extreme summers with hot weather and high peak loads typically have steep load duration curves, meaning that daily peak loads drop quickly relative to the summer peak load on a per-unit basis. Based on this finding, the 2013 load shape is assigned to bins 1 and 2 (upper 6.68% probability of occurrence). The 2013 load shape is reflective of a hot summer peak day and a very high peak load level. The 2018 load shape, reflective of fairly typical peak day weather, is assigned to bins 3 and 4 (62.46% probability of occurrence, including the average load level). Finally, the 2017 load shape, reflective of a mild summer, is assigned to bins 5 through 7 (lower 30.85% probability of occurrence). Figure A.4 shows a comparison of the daily load duration curve for the 2002, 2006, 2007, 2013, 2017, and 2018 summers.

<span id="page-21-0"></span>![](_page_21_Figure_3.jpeg)

#### **Figure A.4 Per Unit Summer Load Shapes**

An additional LFU Phase 2 recommendation was to properly scale the historical load shapes to reflect the increasing capacity of Behind-the-Meter (BTM) solar in future years. BTM solar is not modeled as a supply resource in the 2025-2026 IRM study base case. Therefore, the 2013, 2017, and 2018 historical load shapes were adjusted by scaling up the underlying BTM solar impacts from those years to reflect the load shapes that would result from the projected 2025 BTM solar capacity. The 2025-2026 IRM study thus reflects the average impact of increasing BTM solar penetration on load levels and daily shapes, through use of BTM solar-adjusted historical load shapes.

## **A.3.3 Capacity Model**

The capacity model includes all NYCA generating units, including new and planned units, as well as units that are physically outside New York State that have met specific criteria to offer capacity in the New York Control Area. The 2024 Load and Capacity Data Report (commonly referred to as the "Gold Book") is the primary data source for these resources. Table A.8 provides a summary of the capacity resource assumptions in the 2025-2026 IRM study.

<span id="page-22-0"></span>![](_page_22_Picture_249.jpeg)

## **Table A.8 Capacity Resources**

<span id="page-22-1"></span> $<sup>2</sup>$  The process includes the latest Gold Book publication, NYISO interconnection queue, and generation notifications.</sup>

![](_page_23_Picture_325.jpeg)

![](_page_24_Picture_302.jpeg)

![](_page_25_Picture_219.jpeg)

## (1) Generating Unit Capacities

The capacity rating for each thermal generating unit is based on its Dependable Maximum Net Capability (DMNC). The source of DMNC ratings are seasonal tests required by procedures in the NYISO Installed Capacity Manual. Additionally, each generating resource has an associated Capacity Resource Interconnection Service (CRIS) value. When the associated CRIS value is less than the DMNC rating, the CRIS value is modeled. Wind units are rated at the lower of their CRIS value or their nameplate value in the model. The 2024 Gold Book, issued by the NYISO, is the source of those generating units and their ratings included on the capacity model.

## (2) Planned Generator Units

There are 47 MW of unit re-ratings (summer ratings).

## (3) Wind Modeling

Wind generators are modeled as hourly load modifiers using hourly production data over the period 2019-2023. Each calendar production year represents an hourly wind shape

for each wind facility from which the GE-MARS program will randomly select. New units will use the zonal hourly averages of current units within the same zone. As shown in Table A.9, a total of 2,566.2 MW of installed capacity is associated with wind.

<span id="page-26-0"></span>![](_page_26_Picture_30.jpeg)

## **Table A.9 Wind Generation**

## (4) Solar Modeling

Solar generators are modeled as hourly load modifiers using hourly production data over the period 2019-2023. Each calendar production year represents an hourly solar shape for each solar facility which the GE-MARS program will randomly select from. As shown in Table A.10, a total of 571.4 MW of solar capacity was modeled.

<span id="page-27-0"></span>![](_page_27_Picture_108.jpeg)

## **Table A.10 Solar Generation**

## (5) Retirements/Deactivations/ ICAP Ineligible

There are 6 units totaling 165.4 MW that are being deactivated for the 2025-2026 IRM study.

## (6) Unforced Capacity Deliverability Rights (UDRs)

The capacity model includes UDRs, which are capacity rights that allow the owner of an incremental controllable transmission project to provide locational capacity benefits. Non-locational capacity, when coupled with a UDR to deliver capacity to a Locality, can be used to satisfy locational capacity requirements. The owners of the UDRs elect whether they will utilize their capacity deliverability rights on a confidential basis by August 1<sup>st</sup> for the upcoming Capability Year (*i.e.*, August 1, 2024 for the Capability Year beginning on May 1, 2025). This decision determines how this transfer capability will be

represented in the GE-MARS model. The IRM modeling accounts for both the availability of the resource that is identified for each UDR line as well as the availability of the UDR facility itself. The following facilities are represented in the 2025-2026 IRM study as having UDR capacity rights: LIPA's 330 MW High Voltage Direct Current (HVDC) Cross Sound Cable, LIPA's 660 MW HVDC Neptune Cable, and the 315 MW Linden Variable Frequency Transformer. The owners of these facilities have the option, on an annual basis, of selecting the MW quantity of UDRs they plan on utilizing for capacity contracts over these facilities. Any remaining capability on the cable can be used to support emergency assistance, which may reduce locational and IRM capacity requirements. The 2025-2026 IRM study incorporates the confidential elections that these facility owners made for the 2025-2026 Capability Year. Hudson Transmission Partners 660 MW HVDC Cable has been granted UDR rights but has lost its right to import capacity and therefore is modeled as being fully available to support emergency assistance in Bins 3-7, Bin 1 is modeled with 90 MW and Bin 2 is modeled with 173 MW.

## (7) Energy Limited Resources

The capacity model now includes Energy Limited Resources (ELRs). The NYISO filed, and FERC approved, tariff changes that enhance the ability of duration limited resources to participate in the NYISO markets. These rules allow output limited resources to participate in the markets consistent with those limitations and requires owners of those resources to inform the NYISO of their elected energy output duration limitations. Effective May 1, 2021, generation resources may participate in an ELR program administered by the NYISO. Under this program, participating generators are required to submit their elected limitations to the NYISO on a confidential basis by August  $1<sup>st</sup>$  for the upcoming Capability Year (*i.e.*, August 1, 2024 for the Capability Year beginning on May 1, 2025).

## (8) Performance Data

Performance data for thermal generating units in the model includes forced and partial outages, which are modeled by inputting a multi-state outage model that is representative of the EFORd for each unit represented. Generation owners provide outage data to the NYISO using Generating Availability Data System (GADS) data in accordance with the NYISO Installed Capacity Manual. The NYSRC is continuing to use a five-year historical period for the 2025 IRM study.

Figure A.5 shows a rolling 5-year average of the same data.

Figures A.6 and A.7 show the availability trends of the NYCA broken out by fuel type.

The multi-state model for each unit is derived from five years of historic events if it is available. For units with less than five years of historic events, the available years of event data for the unit is used if it appears to be reasonable. For the remaining years, the unit NERC class-average data is used.

The unit forced outage states for the most of the NYCA units were obtained from the fiveyear NERC GADS outage data collected by the NYISO for the years 2019 through 2023. This hourly data represents the availability of the units for all hours. From this, full and partial outage states and the frequency of occurrence were calculated and put in the required format for input to the GE-MARS program.

Figures A.8 and A.9 show the unit availabilities of the entire NERC fleet on an annual and 5-year historical basis.

**Figure A.5 Five-Year Weighted Annual Average Zonal EFORds**

## New York 5 Year EFORds

<span id="page-30-0"></span>![](_page_30_Figure_2.jpeg)

The resources included in the calculation of these values include thermal, large hydro, wind, solar, landfill gas, and run-of-river resources with CRIS. These values are the average EFORd of NYCA resources except for external resources such as UDR backing generators, firm imports, firm exports, and SCRs.

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<span id="page-31-0"></span>![](_page_31_Figure_0.jpeg)

**Figure A.6 NYCA Annual Weighted Average Availability**

27

<span id="page-32-0"></span>![](_page_32_Figure_0.jpeg)

**Figure A.7 NYCA Five-Year Weighted Average Availability** 

28

<span id="page-33-0"></span>![](_page_33_Figure_0.jpeg)

**Figure A.8 NERC Weighted Annual Average Availability**

\*2023 NERC Class Averages were not posted by the time the FBC Assumptions were finalized. 2022 NERC Class Averages were used for 2023.

<span id="page-34-0"></span>![](_page_34_Figure_0.jpeg)

**Figure A.9 NERC Five-Year Weighted Average Availability**

\*2023 NERC Class Averages were not posted by the time the FBC Assumptions were finalized. 2022 NERC Class Averages were used for 2023.

## (9) Outages and Summer Maintenance

For the 2022-2023 IRM study, planned and scheduled maintenance was removed because it caused excess EOP usage. This had no impact on LOLE or IRM. Like the 2024-2025 IRM study, planned and scheduled maintenance was not modeled for the 2025-2026 IRM study. The nominal 50 MW of summer maintenance, however, remained constant. The amount is nominally divided equally between Zone J and Zone K.

## (10) Gas Turbine Ambient De-rate

Operation of combustion turbine units at temperatures above DMNC test temperature results in reduction in output. These reductions in gas turbine and combined cycle capacity output are captured in the GE-MARS model using de-ratings based on ambient temperature correction curves. Based on the past reviews of historical data, no changes to the existing combined cycle temperature correction curves are proposed by the NYISO staff. These temperature corrections curves, provided by the Market Monitoring Unit of the NYISO, show unit output versus ambient temperature conditions over a range starting at 60 degrees F to over 100 degrees F. Because generating units are required to report their DMNC output at peak or "design" conditions (an average of temperatures obtained at the time of the transmission district previous four like capability period load peaks), the temperature correction for the combustion turbine units is derived for and applied to temperatures above transmission district peak loads.

## (11) Large Hydro De-rates

Hydroelectric projects are modeled consistent with the treatment of thermal units, with a probability capacity model based on five years of unit performance. Except in the case were an election such as ELR status would override the unit being modeled as a thermal unit. See Table A.8 above entitled: Capacity Resources.

## **A.3.4 Transmission System Model**

A detailed transmission system model is represented in the GE-MARS topology. The transmission system topology, which includes eleven NYCA Zones and four External Control Areas, along with transfer limits, is shown in Figure A.10. The transfer limits employed for the 2025-2026 IRM study were developed from emergency transfer limit analyses included in various studies performed by the NYISO and based upon input from Transmission Owners and neighboring regions. The NYISO's Transmission Planning and Advisory Subcommittee (TPAS) and/or NYISO's System Operations Advisory Subcommittee (SOAS) also reviewed and approved the topology. The transfer limits are further refined by other assessments conducted by the NYISO. The assumptions for the transmission model included in the 2025-2026 IRM study are listed in Table A.11, which
reflects changes from last year's model. The changes captured in this year's model include: 1) A proposed update to the West Central reverse limit, aligning with the 2024 Summer Operating Study which reflects changes in load patterns in Zones A and B, with no impact on IRM or LCR; 2) A slight reduction in the Central East forward limit due to the continued outage of the Marcy STATCOM, with no impact on IRM; 3) The UPNY-SENY transfer limit remains unchanged, accounting for the progress of the Dover PAR which is part of Segment B of the AC Transmission project ; 4) Dynamic limit updates from Con Edison's 2023 Local Transmission Plan, resulting in increased export capacity from Staten Island to Load Zone J, with the base export limit remaining unchanged.

Forced transmission outages are included in the GE-MARS model for the underground cables that connect New York City and Long Island to surrounding Zones. The GE-MARS model uses transition rates between operating states for each interface, which were calculated based on the probability of occurrence from the most recent ten years of historic failure rates and the time to repair. Transition rates into the different operating states for each interface were calculated based on the circuits comprising each interface, including failure rates and repair times for the individual cables, and for any transformer and/or phase angle regulator associated with that cable. The applicable Transmission Owners provided updated transition rates for their associated cable interfaces.



## **Table A.11 Transmission System Model**





Table A.12 shows the interface limits including dynamic limits used in the 2025 IRM study topology VS. the 2024 IRM study. **Interface Limits Updates**



#### **Table A.12 2025-2026 IRM Transmission Topology Interface Limits**

The Topology for the 2025-2026 IRM study features the three major changes from the 2024-2025 IRM study.

- 1. Adjustment of the Central East Forward Limit due to Marcy STATCOM Outage:
	- The Central East forward limit has been updated in the 2025 IRM study due to the continued outage of the Marcy STATCOM, which is expected to be out of service until May 2025. The outage impacts the voltage collapse transfer limit by 75 MW. However, there is no impact on the Central East + Marcy South Group (Total East interface) since it remains thermally constrained, meaning the Total East transfer limit is not affected by the STATCOM outage. This update does not impact the IRM
- 2. Update to the West Central Reverse Limit:
	- The West Central reverse limit has been reduced from 2,275 MW to 2,200 MW following the Summer 2024 Operating Study. This change is driven by the

redistribution of flows caused by shifting load patterns in Zones A and B , as well as updates to the thermal ratings of limiting circuits in the region. The adjustment has been tested in the 2024-2025 IRM FBC, with no significant impact on the IRM or MLCRs

- 3. Dynamic Limit Updates for Staten Island to Zone J (New York City):
	- Dynamic limit updates reflecting Con Edison's 2023 Local Transmission Plan (LTP) have resulted in an increased export capability from Staten Island to Load Zone J under certain generator availability conditions. This update enhances the export limits by approximately 200-250 MW in scenarios where capacity unbottling projects on Staten Island are operational.
	- The base export limit from Staten Island to Zone J remains unchanged at 815 MW. However, the dynamic updates provide increased flexibility in managing capacity exports under specific conditions, aligning with the latest assumptions from the 2024 Reliability Needs Assessment (RNA).

#### **External Area Representations**

NYCA reliability depends in part on emergency assistance (EA) from its interconnected Control Area neighbors (New England, Ontario, Quebec and PJM) based on reserve sharing agreements with these external Control Areas. Load and capacity models of these Areas are therefore represented in the GE-MARS analyses with data received directly from the Areas and through NPCC sources.

The primary consideration for developing the final load and capacity models for the external Control Areas is to avoid over-dependence on the external Control Areas for emergency capacity support.

For this reason, a limit is placed on the amount of emergency capacity support that the NYISO can receive from external Control Areas in the IRM study. The 2023-2024 IRM study the limit was 3,500 MW for all LFU bins. For the 2024-2025 IRM study, the EA limit was updated to vary by LFU bin or load level. Based on a study and recommendation from the NYISO<sup>[3](#page-41-0)</sup> that considered the amount of extra reserves that are available in the external Control Areas above an Area's required operating reserve by load level, the 3,500 MW limit was modified as follows: LFU Bin 1: 1,470 MW; LFU Bin 2: 2,600 MW; LFU Bin 3-7: 3,500 MW. Also, Interface limits between the NYISO and neighboring Control Areas were adjusted such that the total EA from all Control Areas does not exceed the EA limit by LFU Bin. During the 2025-2026 IRM study, the dynamic

<span id="page-41-0"></span><sup>3</sup> See [Installed Capacity Subcommittee Meeting No. 278](https://www.nysrc.org/committees/installed-capacity-subcommittee/installed-capacity-subcommittee-schedule-meeting-materials/installed-capacity-subcommittee-meeting-no-278-june-28-2023/) — June 28, 2023 – NYSRC **Agenda Item 9 "**[EOP Review](https://www.nysrc.org/wp-content/uploads/2023/06/9_EOP-Review-Whitepaper-Update18894.pdf)  [Whitepaper Update](https://www.nysrc.org/wp-content/uploads/2023/06/9_EOP-Review-Whitepaper-Update18894.pdf)" and [Installed Capacity Subcommittee Meeting No. 279](https://www.nysrc.org/committees/installed-capacity-subcommittee/installed-capacity-subcommittee-schedule-meeting-materials/installed-capacity-subcommittee-meeting-no-279-august-2-2023/) — August 2, 2023 **Agenda Item 13 "**[EOP](https://www.nysrc.org/wp-content/uploads/2023/08/EOP_Whitepaper_Preliminary_Recommendations_08022023_v1020949.pdf)  [Whitepaper Preliminary Recommendations](https://www.nysrc.org/wp-content/uploads/2023/08/EOP_Whitepaper_Preliminary_Recommendations_08022023_v1020949.pdf) for study details".

emergency assistance modeling was expanded to include the HVDC lines to reflect the proportional limits to emergency assistance from the external control areas.

In addition, an external Control Area's LOLE assumed in the IRM study cannot be lower than its LOLE criteria and its reserve margin can be no higher than its minimum requirement. If the Area's reserve margin is lower than its requirement and its LOLE is higher than its criterion, pre-emergency demand response can be represented. In other words, the neighboring Areas are assumed to be equally or less reliable than NYCA.

Another consideration for developing models for the external Control Areas is to recognize internal transmission constraints within the external Control Areas that may limit emergency assistance to the NYCA. This recognition is considered implicitly for those Areas that have not supplied internal transmission constraint data. Additionally, EOPs are removed from the external Control Area models.

Finally, the top three summer peak load days of an external Control Area should be specified in the load model to be coincident with the NYCA top three peak load days. The purpose of this is to capture the higher likelihood that there will be considerably less load diversity between the NYCA and external Control Areas on the hot summer days.

For this study, both New England and PJM continue to be represented as multi-area models, based on data provided by these Control Areas. Ontario and Quebec are represented as single area models. The load forecast uncertainty model for the outside world model was supplied from the external Control Areas.

Modeling of the neighboring Control Areas in the base case in accordance with Policy 5- 18 is as follows:(see top of next page)



#### **Table A.13 External Area Representations**

Table A.14 shows the final reserve margins and LOLEs for the Control Areas external to NYCA. The 2025 external area model was updated from 2024 but with a modified MW limit for emergency assistance imports during any given hour as described above. As per Table 7-1 of the IRM study report, the difference between the isolated case and the final base case was 5.5% in the 2025 IRM study compared to 6.1% in the 2024 IRM study.



#### **Table A.14 Outside World Reserve Margins**

\*This is the summer margin.

#### **A.3.5 Emergency Operating Procedures (EOPs)**

There are many steps that the system operator can take in an emergency to avoid disconnecting load. EOP steps 2 through 10 listed in Table A.16 were provided by the NYISO based on operator experience. Table A.15 lists the assumptions modeled.

The values in Table A.15 are based on a NYISO forecast that incorporates 2024 (summer) operating results. This forecast is applied against a 2025 peak load forecast of 31,649.7 MW. The table shows the most likely order that these steps will be initiated. The actual order will depend on the type of the emergency. The amount of assistance that is provided by EOPs related to load, such as voltage reduction, will vary with the load level.



#### **Table A.15 Assumptions for Emergency Operating Procedures**



#### **Table A.16 Emergency Operating Procedures Values**

#### **A.3.6 Locational Capacity Requirements**

The GE-MARS model used in the IRM study provides an assessment of the adequacy of the NYCA transmission system to deliver assistance from one Zone to another for meeting load requirements. Previous studies have identified transmission constraints into certain Zones that could impact the LOLE of these Zones, as well as the statewide LOLE. To minimize these potential LOLE impacts, these Zones require a minimum portion of their NYCA ICAP requirement, *i.e.,* locational ICAP, which shall be electrically located within the Zone to ensure that enough energy and capacity are available in that Zone and that NYSRC Reliability Rules are met. For the purposes of the IRM study, locational ICAP requirements are applicable to two transmission-constrained Zones, New York City and Long Island, and are normally expressed as a percentage of each Zone's annual peak load.

These locational ICAP requirements, recognized by NYSRC Reliability Rule A.2 and monitored by the NYISO, supplement the statewide IRM requirement. This report using the unified methodology determines the minimum locational requirements for different levels of installed reserve. The NYSRC chooses the IRM to be used for the coming year and the NYISO chooses the final value of the locational requirements to be met by the LSEs.

#### **A.3.7 Special Case Resources (SCRs)**

SCRs are loads capable of being interrupted, and distributed generators, rated at 100 kW or higher, that are not directly telemetered. SCRs are ICAP resources that only provide energy/load curtailment when activated in accordance with the NYISO Emergency Operating Manual. Performance factors for SCRs are shown in Table A.16:



#### **Table A.17 SCR Performance**

Table A.17 note 1: The SCR performance for 2025-2026 IRM study reflects the "Enhanced SCR Modeling" construct[4](#page-46-0)

GE-MARS model accounts for SCRs as an EOP step and will activate this step before degrading 30-minute reserve capability consistent with the rules for when the program is activated. Both GE-MARS and NYISO operations only activate EOPs in zones where they are capable of being delivered.

SCRs are modeled with monthly values. For the month of July 2024, the registered value is 1,486.7 MW. The effective value of 1,280.8 MW is used in the model.

<span id="page-46-0"></span><sup>4</sup> <https://www.nysrc.org/wp-content/uploads/2024/01/SCR-Modeling-ICS-01302024-Market-Sensitive27154.pdf>

## **A.4 Data Scrub**

### **A.4.1 GE Data Scrub**

General Electric (GE) was asked to review the input data for errors. GE performs a "Data Scrub" which processes the input files and flags data that appears to be out of the ordinary. For example, it can identify a unit with a forced outage rate significantly higher than all the others in that size and type category. If something is found, the NYISO reviews the data and either confirms that it is the right value as is or institutes an update. The results of this data scrub are shown in Table A.18 for the preliminary base case.



#### **Table A.18 GE MARS Data Scrub**

# **A.4.2 NYISO Data Scrub**

The NYISO also performs a review of the MARS data independently from GE. The result of this review is listed below

#### **Table A.19 NYISO Data Scrub**



# **A.4.3 Transmission Owner Data Scrub**

In addition to the above reviews, two transmission owners scrub the data and assumptions using a masked database provided by the NYISO. Their findings are listed below.

#### **Table A.20 Transmission Owner Data Scrub**





# **B. Details for Study Results – Appendix B B.1 Sensitivity Results**

Table B.1 summarizes the 2025-2026 Capability Year IRM requirements under a range of assumption changes from those used for the base case. The base case utilized the computer simulation, reliability model, and assumptions described in Appendix A. The sensitivity cases determined the extent of how the base case required IRM would change for assumption modifications, either one at a time, or in combination. The methodology used to conduct the sensitivity cases was to start with the preliminary base case 23.6% IRM results then add or remove capacity from all zones in NYCA until the NYCA LOLE approached criterion. The values in Table B.1 are the preliminary base case sensitivity results adjusted to the 24.4% final base case IRM.

In addition to showing the IRM requirements for various sensitivity cases, Table B.1 shows the Loss of Load Hours (LOLH) and Expected Unserved Energy (EUE) reliability metrics for each case[.](#page-50-0)<sup>5</sup> These two metrics, along with the LOLE metric, are important measures of reliability risk in that together, they describe the frequency, duration, and magnitude of loss of load events. The reliability risk measures provided by these two metrics, in addition to IRM impacts, provide Executive Committee members with different aspects of system risk for selecting the Final IRM. The data used to calculate LOLH and EUE are collected from GE-MARS output.

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Sensitivity Cases 1 through 5 in Table B.1 are annually performed and illustrate how the IRM would be impacted if certain major IRM study parameters were not represented in the IRM base case.

<span id="page-50-0"></span><sup>5</sup> **LOLH: Loss of Load Hours**: The expected number of hours during loss of load events each year when the system's hourly demand is projected to exceed the generating capacity.

**EUE: Expected Unserved Energy**: The expected amount of energy (MWh) during loss of load events that cannot be served each year**.**

Case 6a examines the impact of reduced oil availability in the winter, reducing the oil capacity to 11,000 MW. Case 6b further reduced the winter oil availability to only 8,000 MW. Case 7 showed the impact of modeling BTM solar resources explicitly as a supply resource. This modeling will allow better understanding of the impact of solar generation on the system.



## **Table B.1 Sensitivity Case Results**



## **Table B.2 Sensitivity Case Results Continued**

Note: All results are calculated by adding/removing capacity from Load Zones A - K unless otherwise noted

## **B.2 Review of LOLE Results and Additional Reliability Metrics**

#### **B.2.1 Review of LOLE Results**

By design, the 2025-26 IRM study final base case (FBC) had an average Loss of Load Expectation (LOLE) of 0.100 events/year. However, that doesn't tell the whole story. The Monte Carlo logic simulated the system for 4,250 replication years and the annual values ranged from a minimum of 0.006 events/year to a maximum of 3.242 events/year. The figure B.1 below shows the value of the LOLE for each of the replication years.



**Figure B.1 Value of LOLE by Replication Year**

The next curve, figure B.2 shows the cumulative average over the course of the replications. After some initial fluctuations the value can be seen to settle out after about 1,500 replications and is fairly constant after 4,250 replications.





The figure B.3 below shows a duration curve of the 4,250 values. While the average value is 0.100 there are hundreds of replications where the value was much higher.



**Figure B.3 LOLE Duration Curve**

#### **B.2.1 Additional Metrics**

In addition to calculating the LOLE in Event-days/year the model also calculated the Hourly Loss of Load Expectation (HLOLE) in Event-hours/year and the Expected Unserved Energy (EUE) in MWH/year. In addition, the expected Duration in hours/event can be determined by dividing the HLOLE by the LOLE and the expected Magnitude in MW/event can be calculated as EUE/HLOLE. Table B.2 below shows the minimum, maximum and average values for these metrics. Although the average duration of outages was roughly 4.2 hours, events of almost 12 hours occurred.





The table B.3 below shows the results broken down by weather year. Although the average LOLE over all of the replications was 0.100 Event-Days/year there were variations by Weather Year. Similar variations can be seen for HLOLE and LOEE in both the average and maximum values. This database uses the last five years of operating history. Further studies planned for next year will look at a longer history.



#### **Table B.3 Results by Weather Year**

The average duration for the replication years ranges from 1.0 hour to 12 hours with an average value of 4.2 hours/event. These are averages over the replication year so they don't capture the full potential range, but they do give a better estimate. As the graph in figure B.4 shows, a 4-hour storage would be insufficient to cover the outage in over 50% of the cases.

#### **Figure B.4 Hours/Event Duration Curve**



In a similar manner the expected Magnitude of the outage was determined for each replication. Although the average was roughly 650 MW over the 4,250 values the maximum exceeded 2300 MW.



#### **Figure B.5 MW/Yr Duration Curve**

Table B.4, below, shows the value of these metrics, along with the Final Base Case IRM, for the past 4 years that they have been recorded. Although the LOLE has remained a constant 0.100 Event-days/year (by design) the IRM has steadily increased but the LOLH and EUE values have bounced around.



#### **Table B.4 IRM Study FBC results for the IRM, LOLH and EUE by Study Yr**

#### **B.2.2 Conclusions**

Although the new calculated and derived metrics add important new insights into the reliability of the system the range of the values across all of the replications adds an even greater dimension. It will be important to calculate not only these new metrics in future studies, but also the distribution of the values for base cases and sensitivities.

## **B.3 Frequency of Implementing Emergency Operating Procedures**

In addition to SCRs, the NYISO will implement several other types of EOPs, such as voltage reductions, as required, to avoid or minimize customer disconnections. Projected 2025 EOP capacity values are based on recent actual data and NYISO forecasts. For the 2025-2026 IRM study, SCR calls were limited to 1 call per day and voluntary load curtailment and public appeals are each limited to 3 calls per year. Table B.5 below presents the expected EOP frequencies for the 2025-2026 Capability Year assuming the 24.4% base case IRM with ELR modeling. Table B.6 presents SCR calls by months.



#### **Table B.5 Implementation of EOP steps**

Note 1: The expected implementation days per year reported in each EOP step are the expected number of days that MARS calls for that EOP step. If an EOP step has a limitation on the number of days that it can provide relief, such as the 3 calls per year for Voluntary Curtailment and Public Appeals, it will provide no load relief after the 3rd call. Starting with the 2025-2026 IRM study year, SCRs have been modeled utilizing a duration limitation with hourly response rates, along with replacing the 5 calls per month limitation with a 1 call per day limitation.

#### **Table B.6 SCR Calls Per Month**





# **Impact of Environmental Regulations**

## **C. Impact of Environmental Regulations- Appendix C**

Federal, state, and local government regulatory programs may impact the operation and reliability of New York's bulk power system. Of note, New York enacted the Climate Leadership and Community Protection Act (CLCPA) and the Accelerated Renewable Energy Growth and Community Benefit Act and promulgated various regulations collectively intended to limit greenhouse gas (GHG) emissions and support the development of new renewable energy, energy storage, and energy efficiency resources. Compliance with state and federal regulatory initiatives and permitting requirements may require investment by the owners of New York's existing thermal power plants to continue in operation. If the owners of those plants must make significant investments to comply, the cost of these investments could lead to retirements, and therefore new resources may be needed to maintain the reliability of the bulk power system. Other regulatory initiatives being undertaken by the State of New York may preclude certain units from continuing in operation in their current configuration. The NYISO executes reliability planning processes to evaluate the implications of resource deactivations or changes in commercial operation. This section reviews the status of various regulatory programs, which may impact power system operations and reliability.

## **C.1 Combustion Turbine NO<sup>X</sup> Emission Limits**

The New York State Department of Environmental Conservation (DEC) Part 227-3 significantly lowers  $NO<sub>X</sub>$  emission limits for simple cycle gas turbines (the "Peaker Rule"). The rule is applicable during the ozone season (May 1- September 30) and establishes lower emission limits in two phases, effective May 1, 2023, and May 1, 2025. The rule requires compliance actions for units with approximately 3,300 MW of capacity (nameplate) located predominantly in southeastern New York and required the owners of affected facilities to file compliance plans by March 2020. The NYISO used compliance plans submitted by generators under Part 227-3 to develop the assumed outage pattern of the impacted units in its Reliability Planning Process.

The 2023 Quarter 2 Short Term Assessment of Reliability (Q2 STAR), which was completed on July 14, 2023, found a reliability need beginning in summer 2025 within New York City primarily driven by a combination of forecasted increases in peak demand and the assumed unavailability of certain generation in New York City affected by the Peaker Rule. $6$  As of May 1, 2023, 1,027 MW of affected generation deactivated or limited their operation. An additional 590 MW of affected generation are expected to become

<span id="page-62-0"></span><sup>&</sup>lt;sup>6</sup> In 2019, the New York State Department of Environmental Conservation adopted a regulation to limit nitrogen oxides (NOx) emissions from simple-cycle combustion turbines, referred to as the "Peaker Rule" ([https://www.dec.ny.gov/regulations/116131.html\)](https://www.dec.ny.gov/regulations/116131.html)

unavailable beginning May 1, 2025, all of which are located in New York City. With the additional generation unavailable, the Q2 Star found that the bulk power transmission system will not be able to securely and reliably serve the forecasted demand in New York City (Load Zone J). Specifically, the New York City zone is deficient by as much as 446 MW for a duration of nine hours on the peak day during expected weather conditions when accounting for forecasted economic growth and policy-driven increases in demand.

The NYISO solicited solutions to address this need in August 2023 with responses provided in early October 2023. On November 20, 2023, after evaluation of the proposals submitted in response to its solicitation, the NYISO determined that no proposals could be installed by May 2025, or were sufficient to address the identified deficiency. As a result, consistent with provisions of the Peaker Rule that permit the NYISO to temporarily retain affected generation if no other solutions are viable or sufficient to address an identified reliability need, the NYISO identified generators on the Gowanus 2 & 3 and Narrows 1 & 2 barges as the temporary solution for the reliability need in New York City. Those generators will remain available for two years beyond the May 1, 2025, deactivation date established by the Peaker Rule.

## **C.2 U.S. Clean Water Act: Best Technology Available for Plant Cooling Water Intake**

The U.S. Environmental Protection Agency (EPA) has issued a new Clean Water Act Section 316b rule providing standards for the design and operation of power plant cooling systems. This rule is being implemented by the DEC, which has finalized a policy for the implementation of the Best Technology Available (BTA) for plant cooling water intake structures. This policy is activated upon renewal of a plant's water withdrawal and discharge permit. Based upon a review of current information available from the DEC, the NYISO has estimated that 13,500 MW of nameplate capacity is affected by this rule, some of which could be required to undertake major system retrofits, including closed-cycle cooling systems.



## **C.3 New York City Residual Oil Elimination**

New York City passed legislation in December 2017 that prohibits the combustion of fuel oil numbers 6 and 4 in electric generators within New York City by 2020 and 2025, respectively. The rule contains an additional compliance pathway providing for conversion directly to fuel oil number 2 by 2023. The rule applies to about 3,000 MW of generation in New York City. Affected generators have filed compliance plans with NYC agencies to switch to compliant fuels. The affected generators are developing new fuel storage and handling equipment necessary to convert their facilities to comply with the law.

## **C.4 Regional Greenhouse Gas Initiative (RGGI)**

RGGI is a multi-state carbon dioxide  $(CO<sub>2</sub>)$  emissions cap-and-trade initiative that requires affected generators to procure emissions allowances authorizing them to emit carbon dioxide. The RGGI states have agreed to a 30% cap reduction between 2020 and 2030, essentially ratcheting down the availability of allowances to generators that emit  $CO<sub>2</sub>$ . The DEC extended RGGI applicability in New York to certain generators of 15 MW (nameplate) or larger in 2021. The current emission allowance caps and design elements are not likely to trigger reliability concerns as the program design provides for mechanisms that consider reliability on various timescales, including multi-year compliance periods,

allowance banking provisions, the Cost Containment Reserve, and periodic program reviews.

The RGGI states are undergoing a third program review. As part of this review, the states are modeling cap trajectories with increased stringency beginning in 2027 and have indicated a preference for moving to annual compliance periods from the current threeyear design. The RGGI States seek feedback to facilitate the integration of additional states that wish to participate in the program. The RGGI states are working to conclude the current program review in early 2025. These proposals have the potential to constrain generator operations if sufficient allowances are not available to the regulated resources, which in certain instances could lead to reliability concerns. Reductions in operational and financial flexibility may need to be recognized by implementing complementary program design elements that can address these concerns.

## **C.5 Distributed Generator NO<sup>X</sup> Emission Limits**

The DEC has adopted Part 222, a rule to limit the NOx emissions from small behind the meter generators that operate as an economic dispatch source in the New York City Metropolitan Area which are located at facilities with potential NOx emissions less than 25 tons of NOx per year and driven by reciprocating or rotary internal combustion engines. The emission limits become effective in two phases, May 1, 2021 and May 1, 2025. Affected facilities must either obtain a registration or permit by March 15, 2021 and must notify the DEC whether the generator will operate as an economic dispatch source subject to the provisions of Part 222.

## **C.6 Cross-State Air Pollution Rule (CSAPR)**

The CSAPR limits emission of  $SO<sub>2</sub>$  and  $NO<sub>X</sub>$  from fossil fuel fired electricity generating units (EGUs) greater than 25 MW in 27 states by establishing emissions caps and restricting allowance trading within various programs. The CSAPR ozone season encompasses May 1-September 30 each year.

The final Revised CSAPR Update became effective June 29, 2021. This rule reduced ozone season  $NO<sub>x</sub>$  limits in 12 of 22 states within the existing Group 2 ozone season trading [program](https://www.epa.gov/airmarkets/final-cross-state-air-pollution-rule-update) by creating a new Group 3. The total 12 state budget decreased by 37% between 2020 and 2021 to 107,085 tons, compared to 2021 emissions of 90,413 tons. Over the same period, the NY budget went down 33% from 5,135 to 3,416 tons, while NY ozone season emissions were 3,550 tons in 2020, 3,997 tons in 2021, 3,506 tons in 2022 and 3,344 tons in 2023. If NY generators emit significantly above their allowable levels the state may collectively exceed its trading limit, in which case higher emitting resources will need to surrender allowances at a rate of 3:1 for their excess emissions.

The EPA [issued](https://www.epa.gov/system/files/documents/2023-03/FRL%208670-02-OAR_Good%20Neighbor_Final_20230314_Signature_ADMIN%20%281%29.pdf) the final Good Neighbor Plan (GNP) for the 2015 Ozone NAAQS on March 15, 2023 expanding the Group 3 region from 12 to 22 states. The [rule](https://www.federalregister.gov/d/2023-05744) became effective August 4, 2023, mid-way through the ozone season. Following legal challenges to the rule, 12 of the 22 states included in Group 3 were removed from the program. These states represented 70% of the program cap. Under the GNP, NY's ozone season  $NO<sub>X</sub>$ budget in 2023-2025 *increased* to 3,912 tons. On June 27, 2024, the Supreme Court of the United States issued a stay of the GNP. The EPA is working to address the court's stay and revert all GNP states back to their prior CSAPR compliance commitments for the 2024 and later ozone seasons. Reverting states to their prior ozone season commitments generally results in an increased  $NO<sub>x</sub>$  emissions cap program wide. However, for New York, reverting to prior commitments will reduce the ozone season cap.

## **C.7 Federal Greenhouse Gas Standards**

The EPA issued final standards for  $CO<sub>2</sub>$  emissions from new combustion turbine and existing steam turbine electric generators which became effective on July 8, 2024. States would submit plans categorizing each existing affected steam turbine generator within 2 years. New natural gas- and oil-fired combustion turbine generators would need to achieve  $CO<sub>2</sub>$  removal rates of 90% beginning in 2032; as would existing coal-fired steam generators that do not commit to cease operations before 2039. New Yorks' existing oiland gas-fired steam turbine generators that frequently operate would be required to maintain historically achieved emissions rate levels. The EPA continues working on a comprehensive rule package to address emissions from existing natural gas- and oil-fired combustion turbine generators which must include options to maintain power system reliability within the regulatory framework.

## **C.8 New York Power Authority Small Gas Turbine Phase Out**

Provisions included in New York State's *2023-24 Enacted State Budget* broadened NYPA's authority to develop renewable energy and required it to phase-out their small natural gas power plants.<sup>[7](#page-66-0)</sup> NYPA is required to publish a plan by May 2025 to phase out the production of electricity from its seven smaller natural gas plants (simple-cycle combustion turbines) in New York City and Long Island totaling 517 MW by December 31, 2030, unless those plants are determined to be necessary for electric system reliability, emergency power service, or energy from other sources that may replace energy from NYPA's affected plants would result in more than a de minimis net increase in emissions within a disadvantaged community. NYPA's plan is required to include recommendations

<span id="page-66-0"></span> $7$  See 2023 Laws of New York, Ch. 56, Part QQ, § 5.

and a proposed strategy to replace some or all of the affected plants with renewable energy systems, if appropriate. The basis for such determinations in NYPA's plan, which are required to be updated at least every two years, must be made publicly available along with the supporting documentation for the determination.

## **C.9 Climate Leadership and Community Protection Act (CLCPA)**

The CLCPA requires, among other things, that 70% of electric energy be generated from renewable resources by 2030 and 100% of electric energy be provided by zero emission resources by 2040. The statute will require the displacement of New York's fossil fuelfired generating fleet with eligible renewable resources and other clean energy resources. During this transition, the NPCC and NYSRC resource adequacy rules will require the New York Control Area to maintain reliability criteria for the New York bulk electric system. In addition, the economy-wide GHG emission reduction requirements necessitate significant electrification of the building and transportation sectors. The CLCPA builds upon programs and targets already established under the Clean Energy Standard (CES) and by other state policies. The combined set of requirements for new resources are described in more detail below. The figure describes the timing and requirements of the major combined clean energy and efficiency policies in New York State.



Source: NYISO

## **C.10 Offshore Wind Development**

The CLCPA requires 9,000 MW of offshore wind (OSW) capacity to be developed by 2035. The New York State Public Service Commission (PSC) has issued several orders directing NYSERDA to procure OSW Renewable Energy Certificates (ORECs) from developers for up to the 9,000 MW offshore wind target. As of October 2024, NYSERDA has executed contracts with Empire 1 (810 MW) and Sunrise (924 MW) offshore wind projects. NYSERDA released the 2024 OSW solicitation in July 2024, with resulting contract awards announcement expected in 2025.

## **C.11 Comprehensive Energy Efficiency Initiative**

The PSC has approved an order containing utility budgets and targets to accelerate energy efficiency savings in New York State through 2025. A portion of the 185 TBtu energy savings target established by the CLCPA will come from directed utility programs to support heat pump adoption, as well as from increased deployment of more conventional utility energy efficiency programs.

## **C.12 Storage Deployment Target**

The CLCPA requires 3,000 MW of energy storage capacity to be developed by 2030. On June 20, 2024, the PSC adopted and updated the statewide deployment goal of 6 GW of energy storage resources by 2030. Under the updated storage roadmap, NYSERDA and the New York State Department of Public Service (DPS) expect roughly half of this goal to be met by behind-the-meter resources while the other half is expected to be gridconnected. DPS reported that 977 MW in energy storage capacity was deployed, awarded, or contracted as of March 31, 2024.

## **C.13 Distributed Solar Program**

The CLCPA requires 6,000 MW of installed distributed solar capacity by 2025. On April 14, 2022, the PSC extended NYSERDA's NY-Sun Program, raising the total distributed solar capacity goal to at least 10,000 MW by 2030. Achievement of these targets has been bolstered by strong growth in BTM solar capacity over recent years, along with a robust pipeline of potential future projects.

## **C.14 Clean Energy Standard (CES)**

The PSC initiated the Renewable Portfolio Standards in 2004 to help support the development of renewable energy resources for New York. In 2016 the PSC combined the Renewable Energy Standard (RES) and a Zero Emission Credit (ZEC) Requirements under a new CES policy. Through the CES, NYSERDA supports the development of new

renewable energy resources, and the continued operation of the upstate nuclear generators through March 2029, by signing Renewable Energy Certificate (REC) and ZEC contracts with generators for the environmental attributes associated with their generation. The PSC issued an Order Modifying the CES on October 15, 2020, to align the existing Clean Energy Standard with the requirements of the CLCPA. Specifically, the order increased the RES from 50% to 70% in 2030 and modified the definition of eligible renewable energy resources to align with the CLCPA. The Order authorized the procurement schedules for Tier 1 and Offshore Wind resources needed to achieve the 2030 mandates. The Order also included a new Tier 4 specifically to recognize incremental renewable energy delivered into Zone J. Tier 4 REC contracts with Champlain Hudson Power Express and Clean Path New York, which were approved on April 14, 2022, have the potential to add approximately 2,500 MW of controllable HVDC connections into New York City.

On July 1, 2024, the Draft Clean Energy Standard Biennial Review found a growing shortfall in expected attainment of the 2030 renewable energy target, primarily due to increased load forecasts and delays in renewable projects achieving commercial operation. NYSERDA and DPS Staff have recommended delaying the RES 70% renewable energy target date to 2033 and expanding annual Tier 1 REC procurements.

## **C.15 Economy-wide Greenhouse Gas Emissions Limits and New York Cap-and-Invest**

The CLCPA includes an approach to accounting for climate impacts of emissions of various GHGs which provide greater weight to the impact of methane emissions relative to the emissions of carbon dioxide and accounts for upstream emissions that occur out-of-state. The 1990 inventory, methodology, and limits were finalized by DEC as Part 496 in 2020.

The DEC is required under the CLCPA to complete additional regulations to enforce the economy wide GHG limits by 2024. Principle among these regulatory initiatives, the DEC and NYSERDA are developing regulations to implement an economy-wide cap-and-invest program to be finalized in 2025 with potential implementation beginning as soon as 2026. The suite of regulatory programs stemming from the Climate Action Council's Final Scoping Plan recommendations will ultimately impact the supply-demand balance in the electric sector.

## **C.16 CLCPA Impact on Air Emission Permits**

In addition, fossil fuel-fired generation projects face further scrutiny under the CLCPA, which requires state agencies to consider consistency with the statewide GHG emission limits and environmental justice impacts when issuing permits.

On October 27, 2021, the DEC denied air emission permit modification applications by two existing generators to repower their facilities with new natural gas generators. The Danskammer Energy Center sought authorization to construct a new natural gas fired combined cycle power generation facility of 536 MW to replace its existing 532 MW generating facility. Astoria Gas Turbine Power, LLC, a subsidiary of NRG Energy, sought to construct the Astoria Replacement Project, which would consist of a new simple cycle dual fuel (natural gas and distillate oil) peaking combustion turbine generator of 437 MW. On June 30, 2022, the DEC also denied the renewal application for Greenidge Generation's air permits citing CLCPA compliance demonstration. The DEC determined that each of the projects would be inconsistent or interfere with the attainment of statewide GHG emission limits established by the CLCPA. The DEC found that the applicants had not provided adequate justification, such as resolution of an electric system reliability need, to overcome the DEC's determination that the air emissions would be inconsistent or interfere with attainment of the CLCPA greenhouse gas emission requirements. The DEC noted at that time, the reliability needs the NYISO identified in its 2020 RNA had been resolved by post RNA updates, and that the announced Tier 4 projects would significantly increase transmission capacity into New York City.

In December 2022, the DEC finalized department program policy DAR-21 to implement the GHG permitting requirements in the CLCPA within state and federal air permits. Facilities are required to submit a GHG Mitigation Plan with their Title V applications addressing climate impacts associated with the facility. On May 8, 2024, the DEC released DEP 24-1 to implement the environmental justice and disproportionate burden aspects of the CLCPA within many environmental permits. For facilities "in or likely to affect" disadvantaged communities (DACs), a Disproportionate Burden Report as well as meaningful community engagement is required under the department policy.

## **C.17 Accelerated Renewable Energy Growth and Community Benefit Act**

The Accelerated Renewable Energy Growth and Community Benefit Act was signed into law on April 3, 2020, to assist in the achievement of the clean energy and environmental targets outlined in the CLCPA. This Act requires the PSC to establish new planning processes to enable the transmission and distribution expansion to support the CLCPA targets. On May 14, 2020, the PSC commenced a proceeding to implement the Act with respect to utility-based plans for upgrades to local transmission and distribution needed to support the mandates of the CLCPA. Utilities submitted preliminary upgrade proposals by August 1, 2020. The Joint Utilities filed an Initial Power Grid Study report at the PSC on November 2, 2020. The report addresses local transmission system needs, existing system planning process and identified some potential modifications to those processes, accounting for CLCPA benefits in planning and investment criteria, and cost containment, cost allocation and cost recovery mechanisms for transmission projects. The PSC subsequently issued orders approving Phase 1 and Phase 2 projects as well as other recommendations stemming from the Power Grid Study, to meet CLCPA requirements. In December 2022, the Joint Utilities filed the Coordinated Grid Planning Process (CGPP) proposal for Commission review. In August 2023, the Commission approved the CGPP with several modifications from what was proposed by the Joint Utilities. The CGPP was designed by the Joint Utilities to assess the transmission needs of the system over a 20 year horizon. The study process is a three-year cycle and includes six stages moving from data collection and modeling and through various stages of capacity expansion and transmission security analysis. The process culminates in a report and recommendations for the Commission's consideration in the identification of transmission projects. The utilities continue working along with the NYISO within the Coordinated Grid Planning Process to identify local transmission and distribution upgrades, coordinate on grid expansion planning and cost sharing. The first cycle of the CGPP began in October 2023 and is expected to conclude in 2026.

The Act also created an Office of Renewable Energy Siting (ORES) within the New York State Department of State to speed the permitting timeline of large-scale renewable energy facilities. Subsequently, the ORES has moved to the DPS and incorporated transmission siting within the same office to help speed the project permitting process. Since 2021, ORES has approved 18 renewable energy projects representing over 2.7 gigawatts.

The Act also directs the PSC and NYSERDA to advance "Build Ready" projects that package project ownership and renewable energy certificate contracts into a single competitive procurement. On October 15, 2020, the PSC issued an order to authorize NYSERDA to begin procurement of Build Ready sites and projects as early as 2022. The program has advanced a 12 MW solar facility at a former mine site to its first request for proposals.

## **C.18 Study Impacts and Insights**

To inform policymakers, market participants, and the public, the NYISO continuously studies the impact of these various policies on the future supply mix. The NYISO's *2023-* 2042 System and Resource Outlook policy scenarios<sup>[8](#page-71-0)</sup> showed the long-term need for

<span id="page-71-0"></span><sup>8</sup> *See* System and Resource Outlook, A Report from the New York Independent System Operator, available at [https://www.nyiso.com/documents/20142/45816558/Outlook-Data-Catalog-2023.pdf/8db92692-9ddb-f91b-fa52](https://www.nyiso.com/documents/20142/45816558/Outlook-Data-Catalog-2023.pdf/8db92692-9ddb-f91b-fa52-e46d0a613202) [e46d0a613202](https://www.nyiso.com/documents/20142/45816558/Outlook-Data-Catalog-2023.pdf/8db92692-9ddb-f91b-fa52-e46d0a613202)
dispatchable emissions-free resources (DEFRs) to operate during extended periods of reduced renewable resource output and to meet winter peak demand needs in an electrified future. These scenarios highlighted the need for resources with these characteristics in addition to energy storage and load flexibility in the potential supply demand balance to address fundamental issues of load and renewable generation misalignment across seasons. The studies also imply increasing ramping demands placed on resources primarily to respond to the increased intermittent output of renewable generation and increased variability of electrified loads.

As outlined in the NYISO's recent Comprehensive Reliability Plan, achieving an emissionfree grid will require DEFRs to be developed and deployed throughout New York. As resources shift from fossil generators to zero emission resources, essential grid services, such as operating reserves, ramping, regulation, voltage support, and black start, must be available to provide New Yorkers with a reliable and predictable electric system that consumers require. DEFRs will be required to provide both energy and capacity over long durations, as well as the reliability attributes of retiring synchronous generation. The attributes do not need to be encapsulated in a singular technology, but in aggregate the system needs a sufficient collection of these services to be reliable.

DEFRs that provide sustained on-demand power and system stability will be essential to meeting policy objectives while maintaining a reliable electric grid. However, while essential to the grid of the future, such DEFR technologies are not commercially viable today. DEFRs will require committed public and private investment in research and development efforts to identify the most efficient and cost-effective technologies with a view towards the development and eventual adoption of commercially viable resources. The development and construction lead times necessary for these technologies may extend beyond policy target dates.



# **D. ICAP to UCAP Translation – Appendix D**

The NYISO administers the capacity requirements to all loads in the NYCA. In 2002, the NYISO adopted the Unforced Capacity (UCAP) methodology for determining system requirements, unit ratings and market settlements. The UCAP methodology uses individual generating unit data for output and availability to determine an expected level of resources that can be considered for system planning, operation and marketing purposes. EFORd is developed from this process for each generating unit and applied to the unit's DMNC test value to determine the resulting level of UCAP.

Individual unit EFORd factors are taken in aggregate on both a Statewide and Locational basis and used to effectively "translate" the IRM and LCRs previously determined in the GE-MARS Analysis in terms of ICAP, into an equivalent UCAP basis.

Table D.1 summarizes the NYCA historical capacity parameters for the last 25 years including Base Case IRMs, approved IRMs, UCAP requirements, and NYISO approved LCRs (for New York City, Long Island and the G-J Locality).



### **Table D.1 Historical NYCA Capacity Parameters**

# **D.1 NYCA and NYC and LI Locational Translations**

In the "Installed Capacity" section of the NYISO website, NYISO staff regularly post summer and winter Capability Period ICAP and UCAP calculations for the NYCA, Localities and Transmission Districts. This information has been compiled and posted since 2006.

Locational ICAP/UCAP calculations are produced for New York City, Long Island, G-J Locality and the entire NYCA. Exhibits D.1.1 through D.1.4 summarizes the translation of ICAP requirements to UCAP requirements for these areas. The charts and tables included in these exhibits utilize data from the summer capability periods for the most recent 15 years beginning in 2009.

This data reflects the interaction and relationships between the capacity parameters used this study, including forecast peak load, ICAP requirements, de-rating factors, UCAP requirements, IRMs, and LCRs. Since these parameters are so inextricably linked to each other, the graphical representation also helps one more easily visualize the annual changes in capacity requirements.

### **D.1.1 New York Control Area ICAP to UCAP Translation**



#### **Table D.2 NYCA ICAP to UCAP Translation**



# **D.1.2 New York City ICAP to UCAP Translation**



### **Table D.3 New York City ICAP to UCAP Translation**



# **D.1.3 Long Island ICAP to UCAP Translation**



#### **Table D.4 Long Island ICAP to UCAP Translation**



# **D.1.4 G-J Locality ICAP to UCAP Translation**



#### **Table D.5 G-J Locality ICAP to UCAP Translation**



# **D.2 Transmission Districts ICAP to UCAP Translation**

### **D.2.1 Central Hudson Gas & Electric**



**Table D.6 Central Hudson Gas & Electric ICAP to UCAP Translation**



## **D.2.2 Consolidated Edison (Con Ed)**



#### **Table D.7 Con Ed ICAP to UCAP Translation**



# **D.2.3 Long Island Power Authority (LIPA)**



### **Table D.8 LIPA ICAP to UCAP Translation**



### **D.2.4 National Grid (NGRID)**



#### **Table D.9 NGRID ICAP to UCAP Translation**



### **D.2.5 New York Power Authority (NYPA)**



### **Table D.10 NYPA ICAP to UCAP Translation**



## **D.2.6 New York State Electric & Gas (NYSEG)**



#### **Table D.11 NYSEG ICAP to UCAP Translation**



### **D.2.7 Orange & Rockland (O & R)**



#### **Table D.12 O & R ICAP to UCAP Translation**



### **D.2.8 Rochester Gas & Electric (RGE)**



### **Table D.13 RGE ICAP to UCAP Translation**



## **D.3 Wind Resource Impact on the NYCA IRM and UCAP Markets**

Wind generation is generally classified as an "intermittent" or "variable generation" resource with a limited ability to be dispatched. The effective capacity of wind generation can be quantified and modeled using the GE-MARS program like conventional fossil-fired power plants. There are various modeling techniques to model wind generation in GE-MARS; the method that ICS has adopted uses historical New York hourly wind farm generation outputs for the previous five calendar years. This data can be scaled to create wind profiles for new wind generation facilities.

For a wind farm or turbine, the nameplate capacity is the ICAP while the effective capacity is equal to the UCAP value. Seasonal variability and geographic location are factors that also affect wind resource availability. For instance, off-shore wind will generally have higher availability and be more coincident with peak load hours than in-land wind. The effective capacity of wind generation can be either calculated statistically directly from historical hourly wind generation outputs, and/or by using the following information:

- $\triangleright$  Production hourly wind data.
- $\triangleright$  Maintenance cycle and duration
- $\triangleright$  EFOR (not related to fuel)

In general, effective wind capacity depends primarily on the availability of the wind. Wind farms in New York on average have annual capacity factors that are based on their nameplate ratings. A wind plant's output can range from close to nameplate under favorable wind conditions to zero when the wind does not blow. On average, a wind plant's output is higher at night, and has higher output on average in the winter versus the summer.

Another measure of a wind generator's contribution to resource adequacy is its effective capacity, which is its expected output during the summer peak hours of 2 p.m. to 6 p.m. for the months of June through August. The effective capacity value for wind generation in New York is based on actual hourly plant output over the previous five-year period – 2019 through 2023 for this year's study, for new units the zonal hourly averages or averages for nearby units will be used. Wind shapes years are selected randomly from those years for each simulation year.

In June 2023 the NYSRC issued a study entitled "Offshore Wind Data Review – NYSRC preliminary findings". This study raises concerns over the correlation in the availability and performance of offshore wind, both internal to the NYCA system, and more importantly across the Northeast region, especially between New York and New England. Currently the

level of offshore wind modeled in the IRM study is low for NYCA and external areas. A study to assess the impact of correlated availability of offshore wind was attempted but showed no impact to the IRM due to only one offshore wind plant being modeled in NYCA and no offshore wind plant modeled in external areas in the IRM base case study database. In addition, the modeling of offshore wind, as well as other intermittent resources, in external areas is not consistent with the IRM approach. Modeling consistency is critical to capture the correlated availability or performance for offshore wind, and capturing such correlation should also be extended to other types of intermittent resources. Therefore, actions are being taken to urge NPCC to establish consistency in modeling and major assumptions across all neighboring systems. Additional sensitivity cases are also being considered for future studies to facilitate monitoring the impact on the IRM as offshore wind penetration increases over time. $9$ 

<span id="page-89-0"></span><sup>9</sup> [https://www.nysrc.org/wp-content/uploads/2023/07/NYSRC-Wind-Impacts-Final-07\\_18\\_23.pdf](https://www.nysrc.org/wp-content/uploads/2023/07/NYSRC-Wind-Impacts-Final-07_18_23.pdf)



# **E. Glossary – Appendix E.**









